

PLATES FOR TENSILE LOADS

TWO VERSIONS

WHT PLATE 440, ideal for framed structures (platform frame);
WHT PLATE 540, ideal for CLT panel structures (Cross Laminated Timber).

PLANAR JOINTS

Ideal for realizing distributed connections under tensile stress between the CLT (Cross Laminated Timber) panels and framed structures (platform frame) to and the concrete understructure.

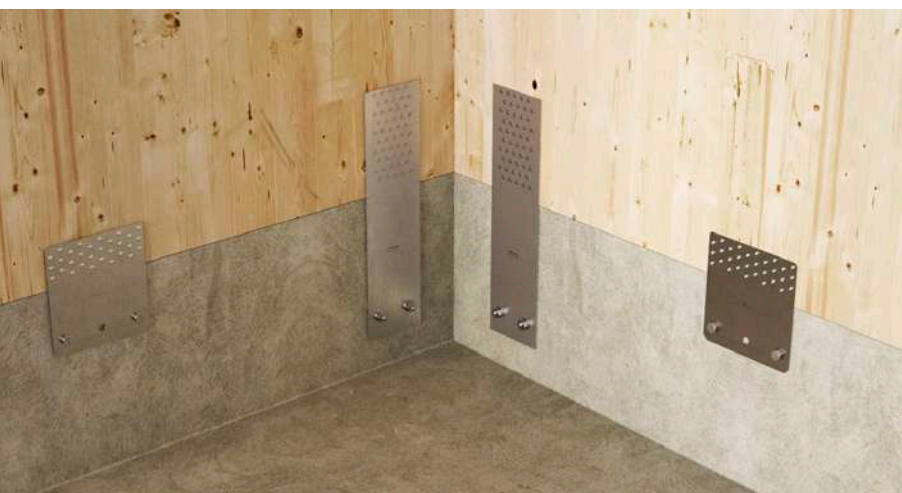
QUALITY

The high tensile strength allows to optimize the number of plates installed, ensuring remarkable time saving.
Values calculated and certified according to CE marking.



CHARACTERISTICS

FOCUS	tensile joints on concrete
HEIGHT	440 540 mm
THICKNESS	3,0 mm
FASTENERS	LBA, LBS, SKR, VIN-FIX PRO, EPO-FIX PLUS



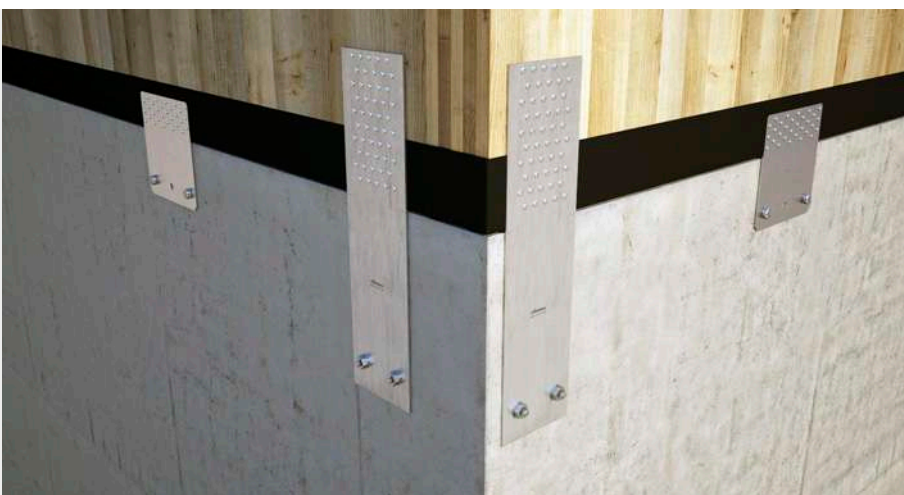
MATERIAL

Bright zinc plated carbon steel, two dimensional perforated plate.

FIELDS OF USE

Timber-to-concrete shear joints for panels and timber struts

- CLT, LVL
- solid timber and glulam
- framed structures (platform frame)
- timber based panels



TIMBER-TO-CONCRETE

Beside its natural function, it is ideal for solving situations where the transfer of tensile loads from timber to concrete is required.

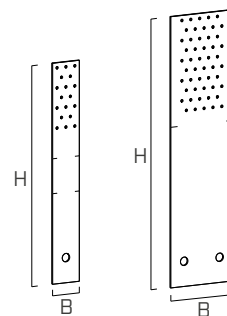
MULTIPURPOSE

Pre-calculated partial nailing can be used if there is a varying amount of stress or a levelling layer.

CODES AND DIMENSIONS

WHT PLATE C

CODE	B	H	holes	$n_v \varnothing 5$	s		pcs
	[mm]	[mm]	[mm]	pcs	[mm]		
WHTPLATE440	60	440	$\varnothing 17$	18	3	●	10
WHTPLATE540	140	540	$\varnothing 17$	50	3	●	10

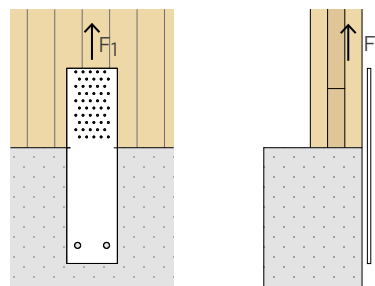


MATERIAL AND DURABILITY

WHT PLATE C: carbon steel DX51D+Z275.

To be used in service classes 1 and 2 (EN 1995-1-1).

EXTERNAL LOADS



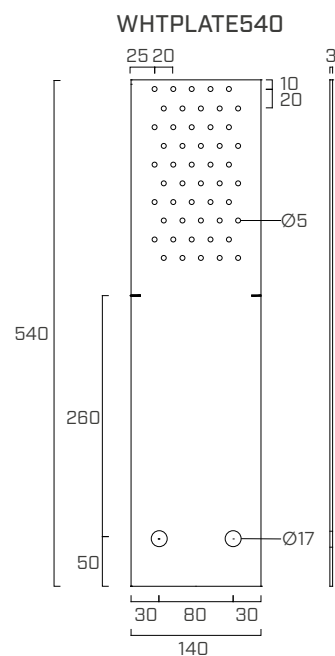
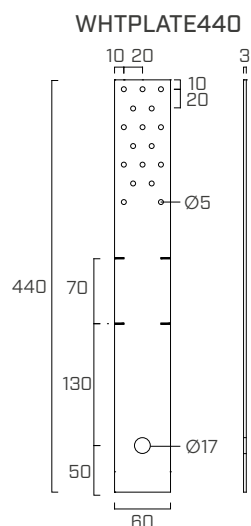
FIELD OF USE

- Timber-to-concrete joints
- OSB-to-concrete joints
- Timber-to-steel joints

ADDITIONAL PRODUCTS - FASTENING

type	description		d	support	page
			[mm]		
LBA	Anker nail		4		548
LBS	screw for plates		5		552
AB1	mechanical anchor		16		494
VIN-FIX PRO	chemical anchor		M16		511
EPO-FIX PLUS	chemical anchor		M16		517
KOS	bolt		M16		526

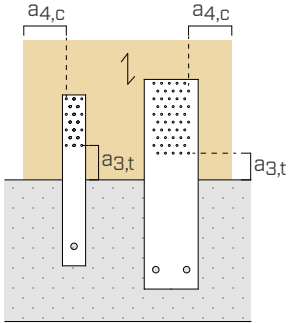
GEOMETRY



INSTALLATION

TIMBER minimum distances		nails LBA Ø4	screws LBS Ø5
C/GL	a _{4,c} [mm]	≥ 20	≥ 25
	a _{3,t} [mm]	≥ 60	≥ 75
CLT	a _{4,c} [mm]	≥ 12	≥ 12.5
	a _{3,t} [mm]	≥ 40	≥ 30

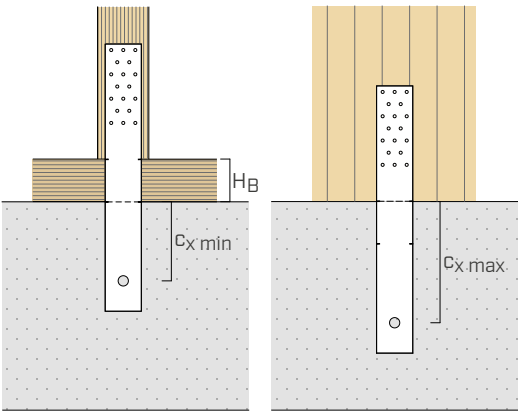
- C/GL: minimum distances for solid timber or glulam consistent with EN 1995-1-1 according to ETA considering a timber density $\rho_k \leq 420 \text{ kg/m}^3$
- CLT: Minimum distances for Cross Laminated Timber according to ÖNORM EN 1995-1-1 (Annex K) for nails and ETA-11/0030 for screws



WHTPLATE440 INSTALLATION

The WHT PLATE 440 can be used for different construction systems (CLT/frame) and ground connection systems (with/without platform beam, with/without levelling layer). Depending on the presence and dimension of H_B of the intermediate layer, in accordance with the minimum distances of the timber and concrete fasteners, the WHT PLATE 440 must be positioned in way that the anchor is at a distance from the concrete edge:

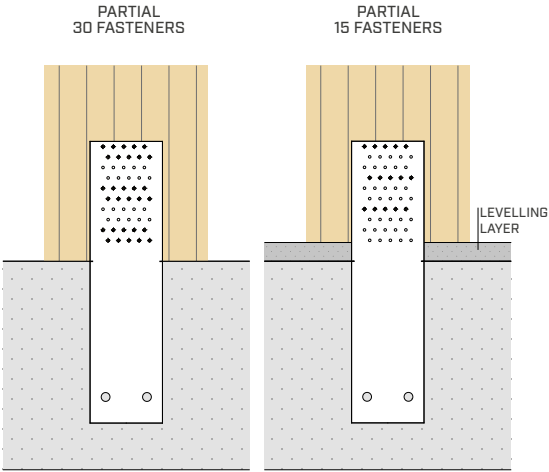
$$130 \text{ mm} \leq c_x \leq 200 \text{ mm}.$$



C_x [mm]	H_B [mm]
$c_{x \text{ min}} = 130$	70
$c_{x \text{ max}} = 200$	0

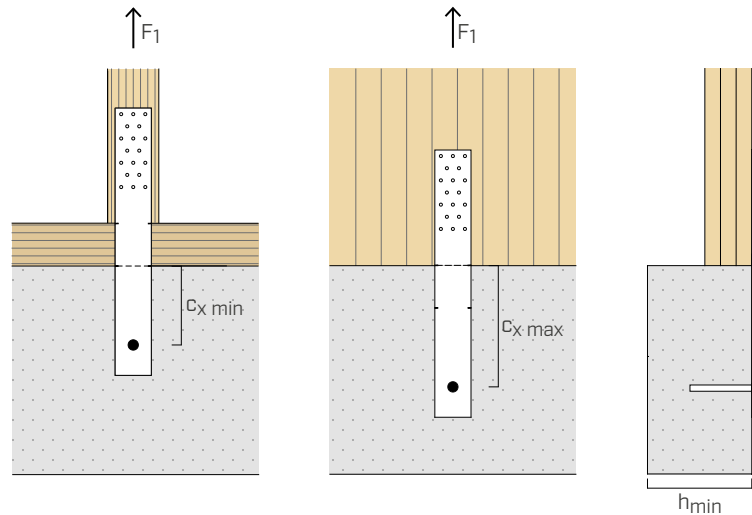
WHTPLATE540 INSTALLATION

In the presence of design requirements such as varying stress values or the presence of a **levelling layer** between the wall and the support surface, it is possible to use pre-calculated and optimised **partial nailing** in order to influence the effective n_{ef} number of fastenings on timber. Alternative nailings are possible in accordance with the minimum distances for the connectors.



■ STATIC VALUES | TENSILE JOINT | TIMBER-TO-CONCRETE

WHTPLATE440



MINIMUM CONCRETE THICKNESS $h_{\min} \geq 200 \text{ mm}$

configuration	R _{1,k} TIMBER				R _{1,k} STEEL		R _{1,d} CONCRETE					
	holes fastening Ø5			R _{1,k} timber [kN]	R _{1,k} steel		R _{1,d} uncracked		R _{1,d} cracked		R _{1,d} seismic	
	type	Ø x L [mm]	n _v [pcs]		[kN]	γ _{steel}	VIN-FIX PRO Ø x L [mm]	[kN]	VIN-FIX PRO Ø x L [mm]	[kN]	EPO-FIX PLUS Ø x L [mm]	[kN]
<ul style="list-style-type: none"> • c_{2 min} = 130 mm • total fastening • 1 anchor M16 	LBA nails	Ø4,0 x 60	18	35,0	34,8	γ _{M2}	M16 x 190	24,8	M16 x 190	17,6	M16 x 190	17,6
	LBS screws	Ø5,0 x 60	18	31,8								
<ul style="list-style-type: none"> • c_{2 max} = 200 mm • total fastening • 1 anchor M16 	LBA nails	Ø4,0 x 60	18	35,0	34,8	γ _{M2}	M16 x 190	31,2	M16 x 190	25,1	M16 x 190	17,6
	LBS screws	Ø5,0 x 60	15 ⁽¹⁾	27,5								

MINIMUM CONCRETE THICKNESS $h_{\min} \geq 150 \text{ mm}$

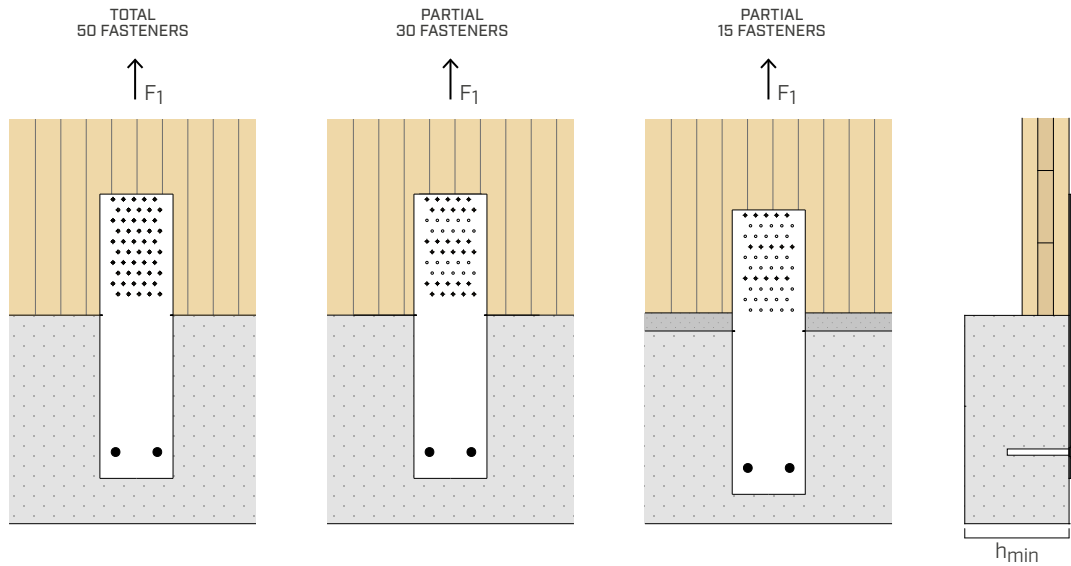
configuration	R _{1,k} TIMBER				R _{1,k} STEEL		R _{1,d} CONCRETE					
	holes fastening Ø5			R _{1,k} timber [kN]	R _{1,k} steel		R _{1,d} uncracked		R _{1,d} cracked		R _{1,d} seismic	
	type	Ø x L [mm]	n _v [pcs]		[kN]	γ _{steel}	EPO-FIX PLUS Ø x L [mm]	[kN]	EPO-FIX PLUS Ø x L [mm]	[kN]	EPO-FIX PLUS Ø x L [mm]	[kN]
<ul style="list-style-type: none"> • c_{2 min} = 130 mm • total fastening • 1 anchor M16 	LBA nails	Ø4,0 x 60	18	35,0	34,8	γ _{M2}	M16 x 136	20,2	M16 x 136	14,3	M16 x 136	14,3
	LBS screws	Ø5,0 x 60	18	31,8								
<ul style="list-style-type: none"> • c_{2 max} = 200 mm • total fastening • 1 anchor M16 	LBA nails	Ø4,0 x 60	18	35,0	34,8	γ _{M2}	M16 x 136	28,8	M16 x 136	20,4	M16 x 136	17,6
	LBS screws	Ø5,0 x 60	15 ⁽¹⁾	27,5								

NOTES:

⁽¹⁾ For the configuration in the table it is recommended not to install the screws of the lower row at a distance of z_{t} (stressed end) = 15d = 75 mm.

■ STATIC VALUES | TENSILE JOINT | TIMBER-TO-CONCRETE

WHTPLATE540



MINIMUM CONCRETE THICKNESS $h_{\min} \geq 200 \text{ mm}$

configuration	R _{1,K} TIMBER				R _{1,K} STEEL		R _{1,d} CONCRETE ^[3]					
	holes fastening Ø5			R _{1,k timber} [kN]	R _{1,k steel}		R _{1,d uncracked}		R _{1,d cracked}		R _{1,d seismic}	
	type	Ø x L [mm]	n _v [pcs]		[kN]	γ _{steel}	VIN-FIX PRO Ø x L [mm]	[kN]	VIN-FIX PRO Ø x L [mm]	[kN]	EPO-FIX PLUS Ø x L [mm]	[kN]
• total fastening • 2 anchors M16	LBA nails	Ø4,0 x 60	50	83,5	70,6	γ _{M2}	M16 x 190	48,2	M16 x 190	34,2	M16 x 190	29,0
	LBS screws	Ø5,0 x 60	50	81,6								
• partial fastening⁽²⁾ 30 fasteners • 2 anchors M16	LBA nails	Ø4,0 x 60	30	70,8								
	LBS screws	Ø5,0 x 60	30	69,9								
• partial fastening⁽²⁾ 15 fasteners • 2 anchors M16	LBA nails	Ø4,0 x 60	15	35,4								
	LBS screws	Ø5,0 x 60	15	35,0								

MINIMUM CONCRETE THICKNESS $h_{\min} \geq 150 \text{ mm}$

configuration	R _{1,K} TIMBER				R _{1,K} STEEL		R _{1,d} CONCRETE ^[3]					
	holes fastening Ø5			R _{1,k timber} [kN]	R _{1,k steel}		R _{1,d uncracked}		R _{1,d cracked}		R _{1,d seismic}	
	type	Ø x L [mm]	n _v [pcs]		[kN]	γ _{steel}	EPO-FIX PLUS Ø x L [mm]	[kN]	EPO-FIX PLUS Ø x L [mm]	[kN]	EPO-FIX PLUS Ø x L [mm]	[kN]
• total fastening • 2 anchors M16	LBA nails	Ø4,0 x 60	50	83,5	70,6	γ _{M2}	M16 x 136	39,6	M16 x 136	28,0	M16 x 136	23,8
	LBS screws	Ø5,0 x 60	50	81,6								
• partial fastening⁽²⁾ 30 fasteners • 2 anchors M16	LBA nails	Ø4,0 x 60	30	70,8								
	LBS screws	Ø5,0 x 60	30	69,9								
• partial fastening⁽²⁾ 15 fasteners • 2 anchors M16	LBA nails	Ø4,0 x 60	15	35,4								
	LBS screws	Ø5,0 x 60	15	35,0								

NOTES:

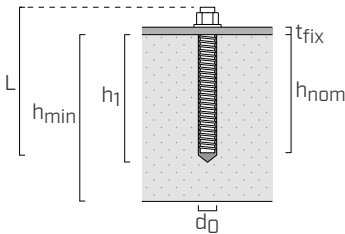
⁽²⁾ In the case of configurations with partial nailing, the strength values in the table are valid for the installation of fasteners in timber in accordance with $a_1 > 10d$ ($n_{ef} = n$)

⁽³⁾ The concrete strength values are valid if the assembly notches of the WHT-PLATE540 plate are positioned at the timber-to-concrete interface ($c_x = 260 \text{ mm}$).

CHEMICAL ANCHORS INSTALLATION PARAMETERS⁽¹⁾

anchor type		t_{fix}	$h_{nom} = h_{ef}$	h_1	d_0	h_{min}
type	$\varnothing \times L$ [mm]	[mm]	[mm]	[mm]	[mm]	[mm]
EPO-FIX PLUS 5.8	M16 x min 136	3	114	120	18	150
VIN-FIX PRO EPO-FIX PLUS 5.8	M16 x 190	3	164	170		200

Precut INA threaded rod, with nut and washer: see page 520
MGS threaded rod class 8.8 to be cut to size: see page 534



t_{fix} fastened plate thickness
 h_{nom} nominal anchoring depth
 h_{ef} effective anchor depth
 h_1 minimum hole depth
 d_0 hole diameter in the concrete support
 h_{min} concrete minimum thickness

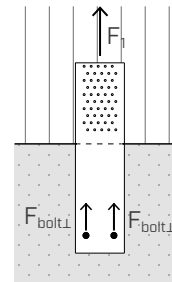
DIMENSIONING OF ALTERNATIVE ANCHORS

Fastening elements to the concrete through anchors not listed in the table, shall be verified according to the load acting on the anchor and evaluable through the coefficients $k_{t\perp}$. The lateral shear load acting on the anchor can be obtained as follows:

$$F_{bolt\perp,d} = k_{t\perp} \cdot F_{1,d}$$

$k_{t\perp}$ coefficient of eccentricity
 F_1 tensile stress acting on the WHT PLATE

	$k_{t\perp}$
WHTPLATE440	1,00
WHTPLATE540	0,50



The anchor check is satisfied if the design tensile strength, obtained considering the boundary effects, is greater than the design external load: $R_{bolt\perp,d} \geq F_{bolt\perp,d}$.

NOTES FOR SEISMIC DESIGN

Particular attention has to be paid to the "capacity design" applied at different scale levels: the global structure and the connection system. Experimentally the ultimate strength of the LBA nail (and of the LBS screw) is notably larger than the characteristic strength evaluated according to EN 1995. E.g. LBA nail $\varnothing 4 \times 60$ mm: $R_{v,k} \approx 2,8 - 3,6$ kN by experimental tests (variable according to the type of timber and plate thickness).

Experimental data derive from tests carried out within the Seismic-Rev research project and are reported in the scientific report: "Connection systems for timber buildings: experimental campaign to characterize stiffness, strength and ductility" (DICAM - Department of Civil, Environmental and Mechanical Engineering - UniTN).



NOTES:

⁽¹⁾ Valid for the strength values shown in the table.

GENERAL PRINCIPLES:

- Characteristic values according to EN 1995-1-1. The design values of the anchors for concrete are calculated in accordance with the respective European Technical Assessments.

The connection design strength value is obtained from the values on the table as follows:

$$R_d = \min \left\{ \begin{array}{l} \frac{R_{k, \text{timber}} \cdot k_{mod}}{\gamma_M} \\ \frac{R_{k, \text{steel}}}{\gamma_{steel}} \\ R_{d, \text{concrete}} \end{array} \right.$$

The coefficients k_{mod} , γ_M and γ_{steel} should be taken according to the current regulations used for the calculation.

- The timber strength values $R_{1,k \text{ timber}}$ are calculated considering the effective number according to Table 8.1 (EN 1995-1-1)

- The calculation process used a timber characteristic density of $\rho_k = 350 \text{ kg/m}^3$ and C25/30 concrete with a thin reinforcing layer and minimum thickness indicated in the relative tables.
- Concrete design strength values are supplied for uncracked ($R_{1,d \text{ uncracked}}$), cracked ($R_{1,d \text{ cracked}}$) concrete and in case of seismic verification ($R_{1,d \text{ seismic}}$) for use of chemical anchor with threaded rod in steel class 5.8.
- Seismic design in performance category C2, without ductility requirements on anchors (option a2 elastic design according to EOTA TR045). For chemical anchors it is assumed that the annular space between the anchor and the plate hole is filled ($d_{gap}=1$).
- The strength values are valid for the calculation hypotheses defined in the table; for boundary conditions different from the ones in the table (e.g. minimum distances from the edge), the anchor-to-concrete group can be verified using MyProject calculation software according to the design requirements.
- Dimensioning and verification of timber and concrete elements must be carried out separately.